

Non-holonomic constraints inducing flutter instability in structures under conservative loadings

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- SUPPLEMENTARY MATERIAL -

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1 Explicit expression for the coefficients ρ_i of the characteristic polynomial for the non-holonomic double pendulum

From Eqs.(58), the explicit expressions for the coefficients ρ_i ($i = 0, \dots, 4$) can be obtained as

$$\rho_0 = \frac{1}{4} \left(\tilde{I}_{r,L} \tilde{M}_L + \frac{1}{16} \tilde{d}^4 + \frac{1}{2} \tilde{d}^2 \tilde{I}_{r,L} + \frac{1}{4} \tilde{d}^2 \tilde{M}_L - \frac{1}{4} \tilde{d} \tilde{M}_L + \frac{1}{2} \tilde{I}_{r,L} + \frac{1}{8} \tilde{M}_L \right), \quad (\text{SM } 1)$$

$$\rho_1 = \frac{1}{64} \left(\frac{5}{3} \tilde{c}_e \tilde{d}^2 - \tilde{c}_e \tilde{d} + \frac{1}{3} \tilde{c}_e \right) + \frac{1}{16} \left(\frac{1}{3} \tilde{c}_e \tilde{M}_L + \tilde{c}_{t,L} \tilde{d}^2 - \tilde{c}_{t,L} \tilde{d} + \frac{1}{2} \tilde{c}_{t,L} \right) + \frac{1}{8} \left(\tilde{c}_{r,L} \tilde{d}^2 + \tilde{c}_{r,L} + 2\tilde{c}_{r,L} \tilde{M}_L + 2\tilde{c}_{t,L} \tilde{I}_{r,L} + 3\tilde{c}_i \tilde{d}^2 + 2\tilde{c}_i \tilde{d} + \tilde{c}_i + 10\tilde{c}_i \tilde{M}_L \right) + 2\tilde{c}_i \tilde{I}_{r,L} + \frac{1}{6} \tilde{c}_e \tilde{I}_{r,L}, \quad (\text{SM } 2)$$

$$\rho_2 = \frac{7}{2304} \tilde{c}_e^2 + \frac{1}{16} \left(\frac{1}{3} \tilde{c}_e \tilde{c}_{t,L} - \tilde{d}^2 \tilde{p}^{\text{QS}} - \tilde{d} \tilde{p}^{\text{QS}} \right) + \frac{1}{8} \left((2 + \tilde{k}_1) \tilde{d}^2 + 3\tilde{c}_e \tilde{c}_i + 1 \right) + \frac{1}{4} \left(\tilde{c}_{r,L} \tilde{c}_{t,L} + 5\tilde{c}_{t,L} \tilde{c}_i + \tilde{d} - \tilde{p}^{\text{QS}} \tilde{M}_L + (4 + \tilde{k}_1) \tilde{M}_L \right) + \frac{1}{6} \tilde{c}_e \tilde{c}_{r,L} - \frac{1}{2} \tilde{I}_{r,L} \tilde{p}^{\text{QS}} + 2\tilde{c}_{r,L} \tilde{c}_i + \tilde{c}_i^2 + (1 + \tilde{k}_1) \tilde{I}_{r,L}, \quad (\text{SM } 3)$$

$$\rho_3 = -\frac{5}{96} \tilde{c}_e \tilde{p}^{\text{QS}} + \frac{8 + \tilde{k}_1}{24} \tilde{c}_e + \frac{1}{4} \left((4 + \tilde{k}_1) \tilde{c}_{t,L} - \tilde{c}_{t,L} \tilde{p}^{\text{QS}} \right) - \frac{1}{2} \tilde{c}_{r,L} \tilde{p}^{\text{QS}} + (1 + \tilde{k}_1) (\tilde{c}_i + \tilde{c}_{r,L}), \quad (\text{SM } 4)$$

$$\rho_4 = \tilde{k}_1. \quad (\text{SM } 5)$$

2 Critical flutter load with a single source of viscosity

2.1 Presence of internal damping \tilde{c}_i

The critical load for flutter in the presence of only the internal damping $\tilde{c}_i = r$ is given by

$$\begin{aligned} & \mathcal{P}_d(\tilde{c}_i, \boldsymbol{\xi}) \\ &= \mathcal{P}_d\left(r, \frac{\pi}{2}, \frac{\pi}{2}, 0, \boldsymbol{\xi}\right) \\ &= 2 \left(\frac{\tilde{d}^4 (2(\tilde{k}_1 - 1)\tilde{k}_1 + 5) + 2\tilde{d}^3 (\tilde{k}_1^2 + 5) + \tilde{d}^2 (16\tilde{I}_{r,L}(\tilde{k}_1(2\tilde{k}_1 - 1) + 3) + \tilde{k}_1^2 + 4(\tilde{k}_1(3\tilde{k}_1 - 2) + 10)\tilde{M}_L + 9)}{(\tilde{k}_1 + 1) (\tilde{d}^2 + \tilde{d} + 8\tilde{I}_{r,L} + 4\tilde{M}_L) (\tilde{d}(3\tilde{d} + 2) + 16\tilde{I}_{r,L} + 10\tilde{M}_L + 1)} \right. \\ & \quad + \frac{4\tilde{d} (4\tilde{I}_{r,L} (\tilde{k}_1^2 + 3) + 2(\tilde{k}_1^2 + \tilde{k}_1 + 5) \tilde{M}_L + 1) + 4 [4\tilde{I}_{r,L} (8\tilde{I}_{r,L} (\tilde{k}_1^2 + 1) - \tilde{k}_1 + 1)]}{(\tilde{k}_1 + 1) (\tilde{d}^2 + \tilde{d} + 8\tilde{I}_{r,L} + 4\tilde{M}_L) (\tilde{d}(3\tilde{d} + 2) + 16\tilde{I}_{r,L} + 10\tilde{M}_L + 1)} \\ & \quad \left. + \frac{[\tilde{M}_L (8\tilde{I}_{r,L} (\tilde{k}_1(3\tilde{k}_1 - 1) + 6) - \tilde{k}_1) + 5(\tilde{k}_1^2 + 4) \tilde{M}_L^2] + 16\tilde{M}_L + 1}{(\tilde{k}_1 + 1) (\tilde{d}^2 + \tilde{d} + 8\tilde{I}_{r,L} + 4\tilde{M}_L) (\tilde{d}(3\tilde{d} + 2) + 16\tilde{I}_{r,L} + 10\tilde{M}_L + 1)} \right) \\ & \quad + \tilde{c}_i^2 \frac{16(\tilde{k}_1 + 1)(\tilde{d}(3\tilde{d} + 2) + 16\tilde{I}_{r,L} + 10\tilde{M}_L + 1)}{(\tilde{k}_1 + 1) (\tilde{d}^2 + \tilde{d} + 8\tilde{I}_{r,L} + 4\tilde{M}_L) (\tilde{d}(3\tilde{d} + 2) + 16\tilde{I}_{r,L} + 10\tilde{M}_L + 1)} \end{aligned} \quad (\text{SM } 6)$$

For $\tilde{c}_i \rightarrow 0$ (or equivalently $r \rightarrow 0$) the limit critical load is given by

$$\begin{aligned}
& \mathcal{P}_d^* \left(\frac{\pi}{2}, \frac{\pi}{2}, 0, \boldsymbol{\xi} \right) \\
&= 2 \left(\frac{\tilde{d}^4 (2(\tilde{k}_1 - 1)\tilde{k}_1 + 5) + 2\tilde{d}^3 (\tilde{k}_1^2 + 5) + \tilde{d}^2 (16\tilde{I}_{r,L}(\tilde{k}_1(2\tilde{k}_1 - 1) + 3) + \tilde{k}_1^2 + 4(\tilde{k}_1(3\tilde{k}_1 - 2) + 10)\tilde{M}_L + 9)}{(\tilde{k}_1 + 1) (\tilde{d}^2 + \tilde{d} + 8\tilde{I}_{r,L} + 4\tilde{M}_L) (\tilde{d}(3\tilde{d} + 2) + 16\tilde{I}_{r,L} + 10\tilde{M}_L + 1)} \right. \\
&\quad + \frac{4\tilde{d} (4\tilde{I}_{r,L} (\tilde{k}_1^2 + 3) + 2 (\tilde{k}_1^2 + \tilde{k}_1 + 5) \tilde{M}_L + 1) + 4 [4\tilde{I}_{r,L} (8\tilde{I}_{r,L} (\tilde{k}_1^2 + 1) - \tilde{k}_1 + 1)]}{(\tilde{k}_1 + 1) (\tilde{d}^2 + \tilde{d} + 8\tilde{I}_{r,L} + 4\tilde{M}_L) (\tilde{d}(3\tilde{d} + 2) + 16\tilde{I}_{r,L} + 10\tilde{M}_L + 1)} \\
&\quad \left. + \frac{[\tilde{M}_L(8\tilde{I}_{r,L}(\tilde{k}_1(3\tilde{k}_1 - 1) + 6) - \tilde{k}_1) + 5 (\tilde{k}_1^2 + 4) \tilde{M}_L^2] + 16\tilde{M}_L + 1}{(\tilde{k}_1 + 1) (\tilde{d}^2 + \tilde{d} + 8\tilde{I}_{r,L} + 4\tilde{M}_L) (\tilde{d}(3\tilde{d} + 2) + 16\tilde{I}_{r,L} + 10\tilde{M}_L + 1)} \right) \quad (\text{SM } 7)
\end{aligned}$$

2.2 Presence of external damping \tilde{c}_e

The critical load for flutter in the presence of only the external damping $\tilde{c}_e = r$ is given by

$$\begin{aligned}
& \mathcal{P}_d(\tilde{c}_e, \boldsymbol{\xi}) \\
&= \mathcal{P}_d \left(r, \frac{\pi}{2}, \frac{\pi}{2}, \frac{\pi}{2}, \boldsymbol{\xi} \right) \\
&= \left(175 \tilde{c}_e^2 \tilde{d}^2 - 105 \tilde{c}_e^2 \tilde{d} + 1120 \tilde{c}_e^2 \tilde{I}_{r,L} + 140 \tilde{c}_e^2 \tilde{M}_L + 35 \tilde{c}_e^2 \right. \\
&\quad - (\tilde{d}(5\tilde{d} - 3) + 32\tilde{I}_{r,L} + 4\tilde{M}_L + 1) \left[1225 \tilde{c}_e^4 + 20160 \tilde{c}_e^2 (3\tilde{d}^2(\tilde{k}_1 - 2) - 2\tilde{d}(\tilde{k}_1 + 3) + 8\tilde{I}_{r,L}(3\tilde{k}_1 - 11) + 2(\tilde{k}_1 - 12)\tilde{M}_L + 5) \right. \\
&\quad \left. + 82944 (\tilde{d}^4(\tilde{k}_1(9\tilde{k}_1 + 64) + 36) + \tilde{d}^3(4\tilde{k}_1(17 - 3\tilde{k}_1) + 72) + 2\tilde{d}^2(8\tilde{I}_{r,L}(\tilde{k}_1(9\tilde{k}_1 + 79) + 66) \right. \\
&\quad \left. + \tilde{k}_1(6\tilde{k}_1\tilde{M}_L + 2\tilde{k}_1 + 196\tilde{M}_L - 13) + 144\tilde{M}_L - 12) + 4\tilde{d}(-24\tilde{I}_{r,L}((\tilde{k}_1 - 4)\tilde{k}_1 - 11) + \right. \\
&\quad \left. + \tilde{k}_1(-2\tilde{k}_1\tilde{M}_L + 38\tilde{M}_L + 5) + 72\tilde{M}_L - 15) + 64\tilde{I}_{r,L}^2(\tilde{k}_1(9\tilde{k}_1 + 94) + 121) + 16\tilde{I}_{r,L}(\tilde{k}_1(6\tilde{k}_1\tilde{M}_L + 206\tilde{M}_L - 15) + 264\tilde{M}_L - 55) + \right. \\
&\quad \left. + 4\tilde{M}_L((\tilde{k}_1(\tilde{k}_1 + 136) + 144)\tilde{M}_L - 5(\tilde{k}_1 + 12)) + 25 \right]^{1/2} + 7200\tilde{d}^4\tilde{k}_1 + 14400\tilde{d}^4 - 3168\tilde{d}^3\tilde{k}_1 + 14976\tilde{d}^3 + 122112\tilde{d}^2\tilde{I}_{r,L}\tilde{k}_1 \\
&\quad + 297216\tilde{d}^2\tilde{I}_{r,L} + 22464\tilde{d}^2\tilde{k}_1\tilde{M}_L + 288\tilde{d}^2\tilde{k}_1 + 87552\tilde{d}^2\tilde{M}_L - 7776\tilde{d}^2 - 29952\tilde{d}\tilde{I}_{r,L}\tilde{k}_1 + 94464\tilde{d}\tilde{I}_{r,L} - 1728\tilde{d}\tilde{k}_1\tilde{M}_L \\
&\quad + 576\tilde{d}\tilde{k}_1 + 32256\tilde{d}\tilde{M}_L + 3168\tilde{d} + 516096\tilde{I}_{r,L}^2\tilde{k}_1 + 1548288\tilde{I}_{r,L}^2\tilde{M}_L + 184320\tilde{I}_{r,L}\tilde{k}_1\tilde{M}_L - 6912\tilde{I}_{r,L}\tilde{k}_1 + 783360\tilde{I}_{r,L}\tilde{M}_L \\
&\quad - 89856\tilde{I}_{r,L} + 20736\tilde{k}_1\tilde{M}_L^2 - 576\tilde{k}_1\tilde{M}_L + 119808\tilde{M}_L^2 - 10368\tilde{M}_L \\
&\quad \left. + 1440 \right) / \left(720 (5\tilde{d}^4 + 4\tilde{d}^3 + 4\tilde{d}^2(26\tilde{I}_{r,L} + 7\tilde{M}_L - 1) + 2\tilde{d}(8\tilde{I}_{r,L} + 2\tilde{M}_L + 1) + 8 (30\tilde{I}_{r,L}\tilde{M}_L + \tilde{I}_{r,L}(64\tilde{I}_{r,L} - 3) + 4\tilde{M}_L^2) - 2\tilde{M}_L) \right) \quad (\text{SM } 8)
\end{aligned}$$

For $\tilde{c}_e \rightarrow 0$ (or equivalently $r \rightarrow 0$), the limit critical load is given by

$$\begin{aligned}
& \mathcal{P}_d^* \left(\frac{\pi}{2}, \frac{\pi}{2}, \frac{\pi}{2}, \boldsymbol{\xi} \right) \\
&= 2 \left[25\tilde{d}^4(\tilde{k}_1 + 2) + \tilde{d}^3(52 - 11\tilde{k}_1) + \tilde{d}^2(8\tilde{I}_{r,L}(53\tilde{k}_1 + 129) + 78\tilde{k}_1\tilde{M}_L + \tilde{k}_1 + 304\tilde{M}_L - 27) \right. \\
&\quad + \tilde{d}(8\tilde{I}_{r,L}(41 - 13\tilde{k}_1) - 6\tilde{k}_1\tilde{M}_L + 2\tilde{k}_1 + 112\tilde{M}_L + 11) + 1792\tilde{I}_{r,L}^2(\tilde{k}_1 + 3) + 8\tilde{I}_{r,L}(80\tilde{k}_1\tilde{M}_L - 3\tilde{k}_1 + 340\tilde{M}_L - 39) \\
&\quad \left. + 8(9\tilde{k}_1 + 52)\tilde{M}_L^2 - 2(\tilde{k}_1 + 18)\tilde{M}_L + 5 - (5\tilde{d}^2 - 3\tilde{d} + 32\tilde{I}_{r,L} + 4\tilde{M}_L + 1) \left\{ \tilde{d}^4 (9\tilde{k}_1^2 + 64\tilde{k}_1 + 36) \right. \right. \\
&\quad + \tilde{d}^3 (-12\tilde{k}_1^2 + 68\tilde{k}_1 + 72) + 2\tilde{d}^2 (8\tilde{I}_{r,L} (9\tilde{k}_1^2 + 79\tilde{k}_1 + 66) + \tilde{k}_1^2(6\tilde{M}_L + 2) + \tilde{k}_1(196\tilde{M}_L - 13) + 144\tilde{M}_L - 12) \\
&\quad - 4\tilde{d} (24\tilde{I}_{r,L} (\tilde{k}_1^2 - 4\tilde{k}_1 - 11) + 2\tilde{k}_1^2\tilde{M}_L - \tilde{k}_1(38\tilde{M}_L + 5) - 72\tilde{M}_L + 15) + 64\tilde{I}_{r,L}^2 (9\tilde{k}_1^2 + 94\tilde{k}_1 + 121) \\
&\quad \left. + 16\tilde{I}_{r,L} (6\tilde{k}_1^2\tilde{M}_L + \tilde{k}_1(206\tilde{M}_L - 15) + 264\tilde{M}_L - 55) + 4\tilde{k}_1^2\tilde{M}_L^2 + 544\tilde{k}_1\tilde{M}_L^2 - 20\tilde{k}_1\tilde{M}_L + 576\tilde{M}_L^2 - 240\tilde{M}_L \right. \\
&\quad \left. + 25 \right\}^{1/2} \Big] / \left[5 (5\tilde{d}^4 + 4\tilde{d}^3 + 4\tilde{d}^2(26\tilde{I}_{r,L} + 7\tilde{M}_L - 1) + 2\tilde{d}(8\tilde{I}_{r,L} + 2\tilde{M}_L + 1) + 512\tilde{I}_{r,L}^2 + 24\tilde{I}_{r,L}(10\tilde{M}_L - 1) + 2\tilde{M}_L(16\tilde{M}_L - 1)) \right] \quad (\text{SM } 9)
\end{aligned}$$

3 Critical flutter load with two sources of viscosity

3.1 Presence of internal and external damping

For the sake of simplicity, the critical load is particularized for the case $\hat{\xi} = [1/2, 15, 15, 50]$. By setting $\tilde{c}_e = r \sin \phi_3$, $\tilde{c}_i = r \cos \phi_3$ and $r = \sqrt{\tilde{c}_e^2 + \tilde{c}_i^2}$ the critical load is given by

$$\begin{aligned} \mathcal{P}_d \left(r, \frac{\pi}{2}, \frac{\pi}{2}, \phi_3, \hat{\xi} \right) = & \left[25235r^2 \sin^2 \phi_3 + 3554600r^2 \sin \phi_3 \cos \phi_3 + 96 (240r^2 \cos^2 \phi_3 (6284 \cot \phi_3 + 2717) \right. \\ & + 288 \cot \phi_3 (57927483 \cot \phi_3 + 10504342) + 120487001) \\ & - (12568 \cot \phi_3 + 721) \{ 1225r^4 \sin^4 \phi_3 + 1152 (4225r^4 \sin^2(2\phi_3) + 35552208708) \\ & + 132710400r^4 \cos^4 \phi_3 + 99532800r^4 \sin \phi_3 \cos^3 \phi_3 + 359009280r^2 \sin^2 \phi_3 \\ & - 9953280r^2 \cos^2 \phi_3 (294984 \cot \phi_3 + 98747) + 302400r^2 \sin \phi_3 \cos \phi_3 (r^2 \sin^2 \phi_3 + 117036) \\ & \left. + 1439244288 \cot \phi_3 (11283138 \cot \phi_3 - 711833) \}^{\frac{1}{2}} \right] / [60(54519984 \cot \phi_3 + 2826493)] \end{aligned} \quad (\text{SM } 10)$$

Moreover, the maximum value of the critical limit load (79) can be obtained by taking the limit of vanishing viscosities along the particular direction

$$\bar{\phi}_3 = 2 \tan^{-1} \left(\frac{\sqrt{15690571665841035300\sqrt{120482} + 26294588465714004524410} - 52150850614 - 150434475\sqrt{120482}}{144389423358} \right)$$

and corresponding in this case to the critical value for the ideal case without damping $\mathcal{P}_0(\hat{\xi})$, namely

$$\mathcal{P}_d^* \left(\frac{\pi}{2}, \frac{\pi}{2}, \bar{\phi}_3, \hat{\xi} \right) = \frac{20}{723} \left(3102 - \sqrt{120482} \right) = \mathcal{P}_0 \left(\hat{\xi} \right) \quad (\text{SM } 11)$$

3.2 Presence of translational and rotational damping for the non-holonomic constraint

For the sake of simplicity, the critical load is particularized to the case $\hat{\xi} = [1/2, 15, 15, 50]$. By setting $\tilde{c}_{r,L} = r \sin \phi_1$, $\tilde{c}_{t,L} = r \cos \phi_1$ and $r = \sqrt{\tilde{c}_{r,L}^2 + \tilde{c}_{t,L}^2}$ the critical load is given by

$$\begin{aligned} \mathcal{P}_d \left(r, \phi_1, 0, 0, \hat{\xi} \right) = & \left[-4 \sin(2\phi_1) (r^2 (732 \sin(2\phi_1) - 259 \cos(2\phi_1)) + 741r^2 + 6641121) + 440805 \cos(2\phi_1) - 18295539 \right. \\ & + 2(250 \sin \phi_1 + 241 \cos \phi_1) \{ 64r^4 \sin^2 \phi_1 \cos^4 \phi_1 + \cos^2 \phi_1 (256r^4 \sin^4 \phi_1 + 155027401) \\ & + 2 \sin(2\phi_1) (8r^2 \sin(2\phi_1) (2r^2 \sin(2\phi_1) + 2823) - 52890047) + 183984r^2 \sin \phi_1 \cos^3 \phi_1 \\ & \left. - 374592r^2 \sin^3 \phi_1 \cos \phi_1 + 161137636 \sin^2 \phi_1 \}^{\frac{1}{2}} \right] / [-288272 \sin(2\phi_1) + 6534 \cos(2\phi_1) \\ & - 234538] \end{aligned} \quad (\text{SM } 12)$$

Moreover, the maximum value of the critical flutter load at vanishing viscosity, equation (81), can be obtained as

$$\bar{\phi}_1 = 2 \tan^{-1} \left(\frac{\sqrt{5012544564868560760800\sqrt{120482} + 124334748418387567120122197} - 315372600\sqrt{120482} - 7947019755154}{7820974511191} \right)$$

which corresponds to the critical value for the ideal case without damping $\mathcal{P}_0(\hat{\xi})$, namely

$$\mathcal{P}_d^* \left(\bar{\phi}_1, 0, 0, \hat{\xi} \right) = \frac{20}{723} \left(3102 - \sqrt{120482} \right) = \mathcal{P}_0 \left(\hat{\xi} \right) \quad (\text{SM } 13)$$